

Qspice - Bode Frequency Response Analysis (.bode)

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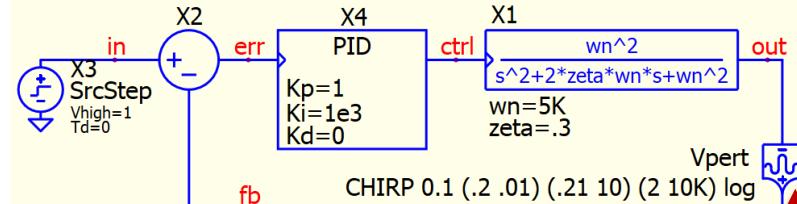
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Concept of Frequency Response Analysis (FRA)

Qspice : Bode - Sine Wave Excitation.qsch

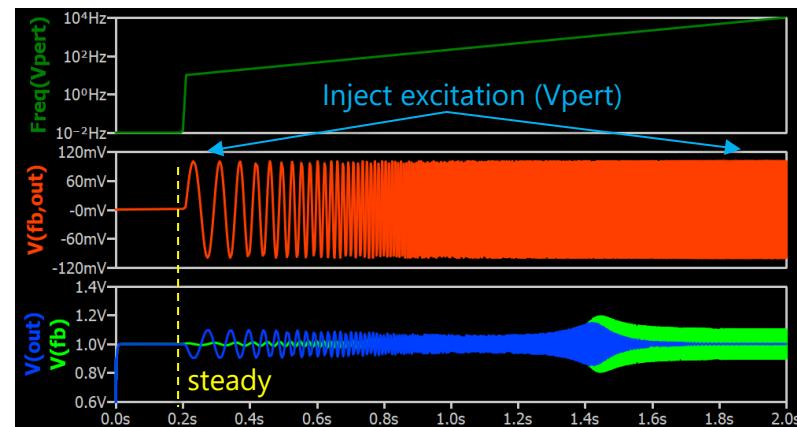
- Frequency Response Analysis (FRA)
 - This is an example of frequency response analysis (FRA) in close-loop system with perturbing source inject into feedback path
 - Perturbing source signal is injected after the system has settled to a steady state
 - This perturbing source can be a sine wave or square wave (step response) in Qspice
 - This excitation can assist in calculating the transfer function between any two nodes affected by this excitation
 - User need to determine system test parameters like Tsettle, start and stop frequencies, perturbing type and amplitude etc., to simulate a time domain waveform for calculating transfer function of between bode output and input nodes

Example of Sine Wave Excitation / Perturbing Source into close-loop system



.tran 2
.plot V(fb) V(out)
.plot V(fb,out)
.plot Freq(Vpert)

I made a special symbol, but this is just a build-in voltage source



Qspice - Bode Frequency Response Analysis (.bode)

- Frequency Response Analysis (.bode)

- Help in Qspice : HELP > Simulator > Command Reference > Frequency Response Analysis (.bode)
- A perturbing voltage source can be inserted in the input (open loop) or feedback path (close loop)
- Both terminals of this perturbing voltage source must not be grounded
- Syntax:**

.bode <SOURCE> <TSETTLE> [<FSTART> [<FSTOP> [<AMP>]]] [SQUARE=<value>] [DEBUG]

- .bode is time domain analysis with perturbing voltage source <SOURCE> generates signal from frequency <FSTART> to <FSTOP> with fixed or variable [.options Bodeampfreq / BodeLoPow / BodeHiPow] amplitude <AMP>. It only collect time domain data after circuit settle to steady state <TSETTLE>
- Simulator performs frequency/phase analysis/deconvolution between output node [.options BODEOUT] and input node [.options BODEIN], and store results into *OpenLoopGain* or *TransferFunction*

.option

Name	Description	Default
BODEAMPFREQ	Frequency with the minimum perturbation amplitude. Set to 0. for constant amplitude.	(not set)
BODEHIPOW	Controls perturbation amplitude for above BODEAMPFREQ by pow (freq/BODEAMPFREQ, BODEHIPOW)	1.
BODEINPUT ¹	Override input node for transfer function computation(AKA BODEIN)	auto
BODELOPOW	Controls perturbation amplitude for below BODEAMPFREQ by pow (freq/BODEAMPFREQ, BODELOPOW)	1.
BODEPERIODS	Maximum number of periods to include in deconvolution	20
BODEREF	Reference node to use for Frequency Response Analysis	Node 0 (global ground)
BODEOUTPUT ¹	Override output node for transfer function computation(AKA BODEOUT)	auto
BODETOL	A Frequency Response Analysis relative tolerance	10.

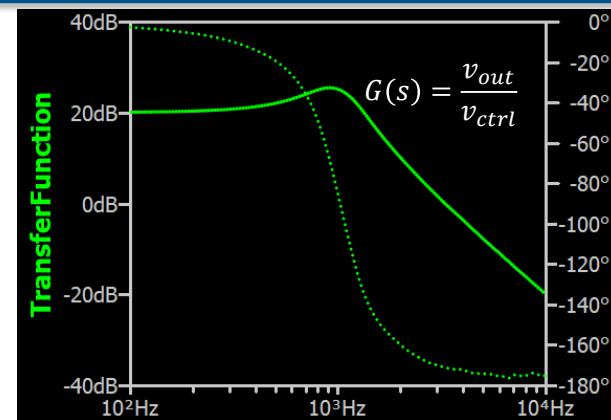
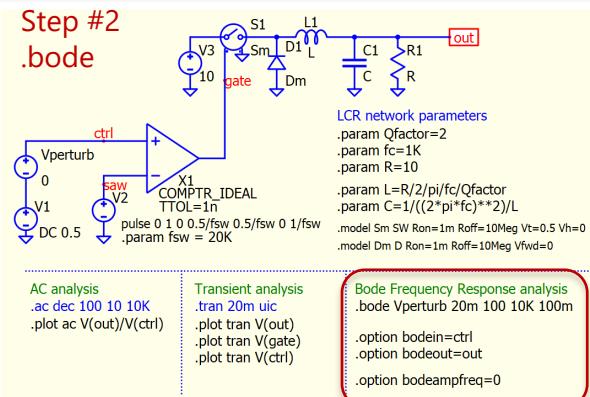
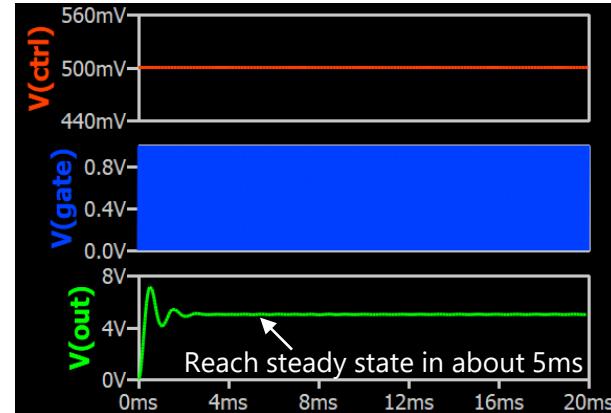
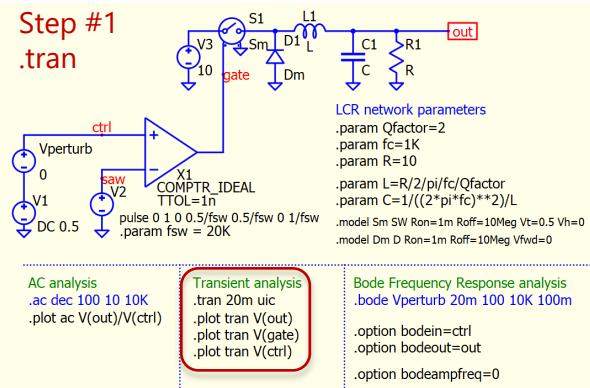
Syntax

Name	Description	Default
SOURCE ²	Name of the perturbing voltage source inserted in the loop	No default but a value is required
TSETTLE ³	Time required for the circuit to settle to steady state	No default but a value is required
FSTART ⁴	Lowest frequency to analyze	1kHz
FSTOP	Highest frequency to analyze	1000 × FSTART
AMP ⁵	Minimum amplitude of perturbing source	2mV ⁶
SQUARE ⁷	Number of square wave periods to average	0
DEBUG	Keep the time domain waveform data	not set

Basic Workflow of using .bode

Qspice : Bode - Buck - transfer function (sine).qsch

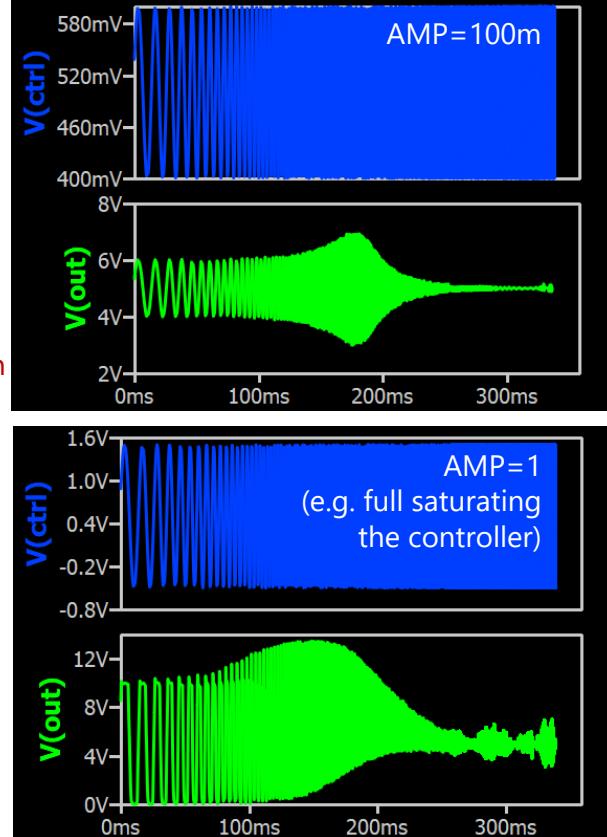
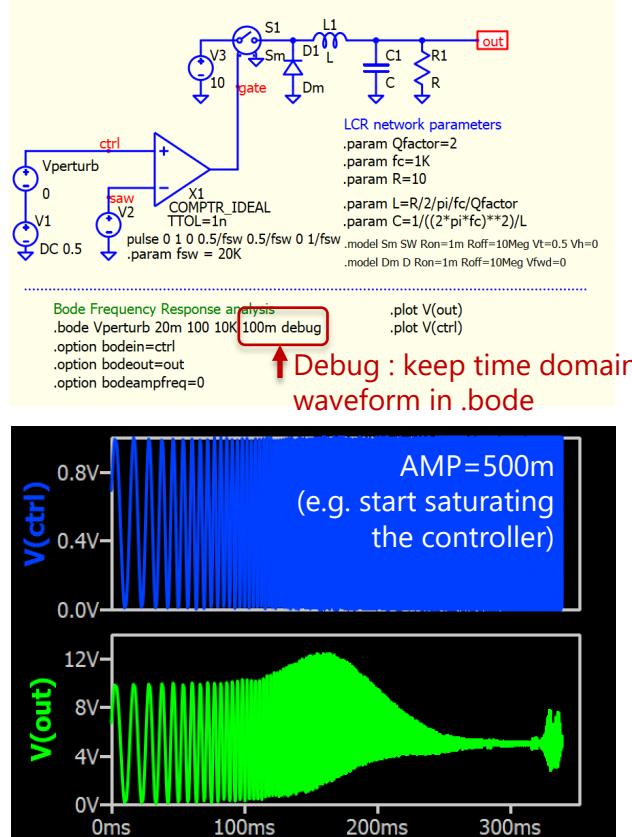
- Identify <Tsettle> with .tran
 - [1] Use .tran to identify settling time for system to reach steady state
- Setup .bode with
 - [2] Add perturbing source to a suitable position
 - both terminals must not be grounded
 - [3] Set <Tsettle> larger than steady state time found in [1]
 - [4] User determine <Fstart> and <Fstop>
 - Within 3 decade and prevent <Fstart> from very low frequency to have reasonable simulation time
 - [5] Determine Transfer Function by specifying in and out node
 - .option bodein=<input node>
 - .option bodeout=<output node>
 - $\text{TransferFunction} = \frac{\text{bodeout}}{\text{bodein}}$
 - [6] Determine perturbing amplitude
 - <amp> set to a proper value
 - .option bodeampfreq=0 can force a constant perturbing amplitude**
(recommend to use this as initial run)



Basic Workflow of using .bode – Determine AMP with Debug

Qspice : Bode - Buck - transfer function (sine-debug).qsch

- AMP and Debug
 - It is necessary to determine amplitude profile that does not saturate the controller but can excite to a useful level for gain/phase calculation
 - **DEBUG** in .bode directive keep time domain waveform for users to observe how to adjust the amplitude (AMP)
 - Users may need to adjust Bodeampfreq / BodeLoPow / BodeHiPow in .option to optimize amplitude at different frequencies to achieve the best signal resolution



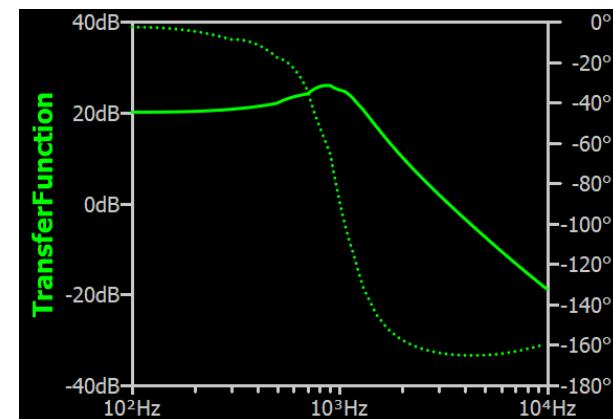
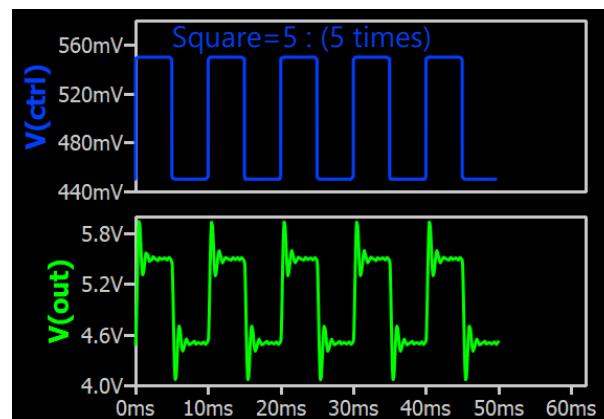
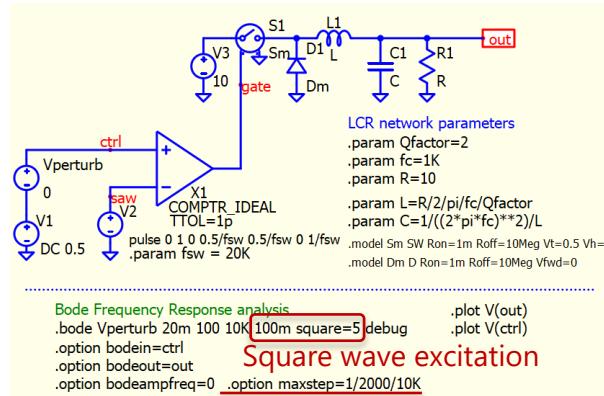
Basic Workflow of using .bode (Sine Wave Excitation)

- .bode simulation process with sine wave excitation
 - .tran simulation with CHIRP as perturbing source
 - Time to achieve steady state : $\langle TSETTLE \rangle$
 - Perturbing source name : $\langle SOURCE \rangle$
 - Perturbing source frequency range : $\langle FSTART \rangle$ and $\langle FEND \rangle$
 - Perturbing source amplitude
 - *.option BODEAMPFREQ*: to determine $\langle AMP \rangle$ min amplitude frequency ($\neq 0$) or constant amplitude ($= 0$)
 - *.option BodeLoPow* and *.option BodeHiPow*: to determine amplitude vs frequency profile
 - Relative tolerance : *.option BODETOL*
 - A lower value results in a longer perturbing source .tran duration, providing higher resolution across frequencies (beneficial for high Q response)
 - Deconvoluting time domain data with 9 threads
 - INPUT and OUTPUT nodes : *.option BODEIN* and *.option BODEOUT*
 - $$\text{TransferFunction} = \frac{\text{bodeout}}{\text{bodein}}$$
 - OUTPUT nodes reference : *.option BODEREF* (default = Node 0 = GND)
 - Maximum deconvolution periods : *.option BODEPERIODS*
 - Applying aperture diffraction corrections

Excitation : Square Wave Excitation

Qspice : Bode - Buck - transfer function (square-debug).qsch

- Square
 - Square=<Number of square wave periods to average>
 - If Square is set to a positive number, a method based on square wave excitation is used
 - A pulse source is used for excitation with peak-to-peak = AMP
 - .option maxstep can be used to increase time step resolution, and therefore, to increase transfer function resolution



Basic Workflow of using .bode (Square Wave Excitation)

- .bode simulation process with square wave excitation
 - .tran simulation with PULSE as perturbing source
 - Time to achieve steady state : $\langle TSETTLE \rangle$
 - Perturbing source name : $\langle SOURCE \rangle$
 - Perturbing source frequency range : $\langle FSTART \rangle$ and $\langle FEND \rangle$
 - Perturbing source amplitude (pulse peak-to-peak) : $\langle AMP \rangle$
 - System identification from time domain data
 - INPUT and OUTPUT nodes : *.option BODEIN* and *.option BODEOUT*
 - $\text{TransferFunction} = \frac{\text{bodeout}}{\text{bodein}}$
 - OUTPUT nodes reference : *.option BODEREF* (default = Node 0 = GND)
 - Improve resolution of system transfer function calculation
 - Limit and reduce maxstep : *.option maxstep*
 - Higher timestep resolution in time domain waveform can improve resolution of system transfer function
 - .option **NOT USED** in square wave excitation
 - *BodeAmpFreq, BodeLoPow, BodeHiPow, BodeTol, BodePeriods*

**Study of syntax and
.option parameters in
.bode**

.bode Syntax and .Option

syntax

Name	Description	Default
SOURCE ²	Name of the perturbing voltage source inserted in the loop	No default but a value is required
TSETTLE ³	Time required for the circuit to settle to steady state	No default but a value is required
FSTART ⁴	Lowest frequency to analyze	1kHz
FSTOP	Highest frequency to analyze	$1000 \times FSTART$
AMP ⁵	Minimum amplitude of perturbing source	2mV ⁶
SQUARE ⁷	Number of square wave periods to average	0
DEBUG	Keep the time domain waveform data	not set

.option

Name	Description	Default
BODEAMPFREQ	Frequency with the minimum perturbation amplitude. Set to 0. for constant amplitude.	(not set)
BODEHIPOW	Controls perturbation amplitude for above BODEAMPFREQ by pow (freq/BODEAMPFREQ, BODEHIPOW)	1.
BODEINPUT ¹	Override input node for transfer function computation(AKA BODEIN)	auto
BODELOPOW	Controls perturbation amplitude for below BODEAMPFREQ by pow (freq/BODEAMPFREQ, BODELOPOW)	1.
BODEPERIODS	Maximum number of periods to include in deconvolution	20
BODEREF	Reference node to use for Frequency Response Analysis	Node 0 (global ground)
BODEOUTPUT ¹	Override output node for transfer function computation(AKA BODEOUT)	auto
BODETOL	A Frequency Response Analysis relative tolerance	10.

Hint

- Normally not need to change Bodeltol (except for high Q frequency response) and Bodeperiods
- First run set BodeAmpFreq=0 for constant amplitude perturbation
- Fstart and Fstop within 3 decade, and Fstart doesn't set at very low frequency
- To improve overall profile, may require varying perturbation amplitude, which requires use of Bodeampfreq / Bodehipow / Bodelipow for amplitude user defined amplitude profile.

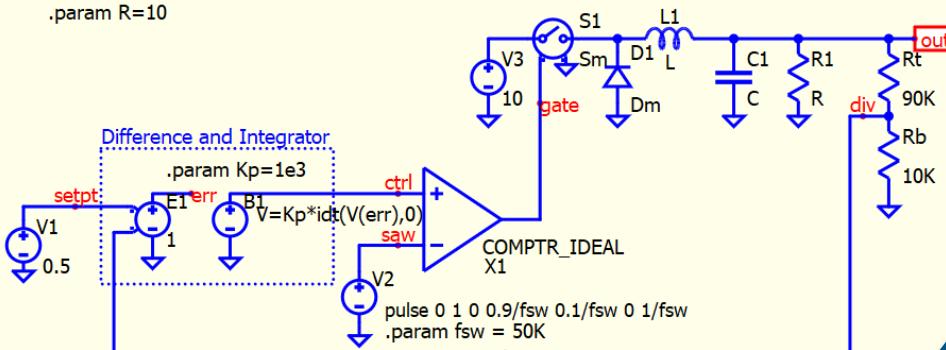
Syntax <SOURCE>

Qspice : bode - Source.qsch

- <Source> can be voltage source or top resistor

- If bodein and bodeout are not defined in .option
- <Source> as voltage source : $OpenLoopGain = \frac{-ve\ terminal\ node}{+ve\ terminal\ node}$
- <Source> as top resistor : $OpenLoopGain = \frac{resistor\ net\ 1\ node}{resistor\ net\ 2\ node} \times \frac{R_{top}}{R_{top} + R_{bottom}}$

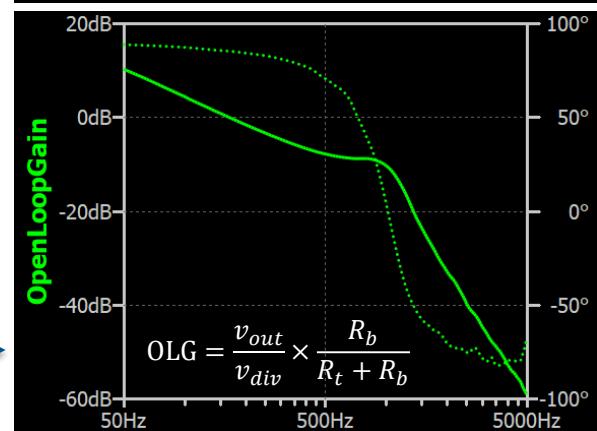
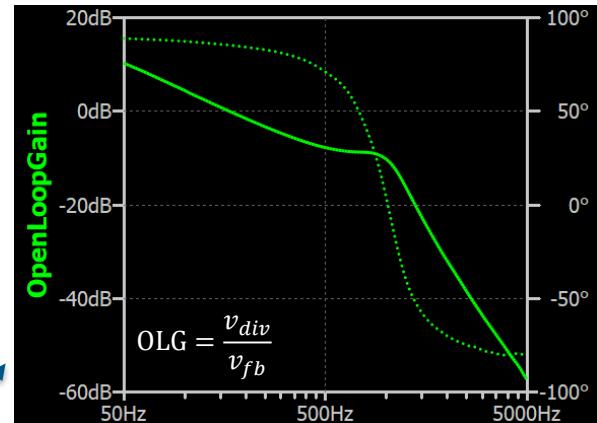
```
.param Qfactor=2      .param L=R/2/pi/fc/Qfactor
.param fc=1K          .param C=1/((2*pi*fc)**2)/L
.param R=10           .model Sm SW Ron=1m Roff=10Meg Vt=0.5 Vh=0
                      .model Dm D Ron=1m Roff=10Meg Vfwd=0
```



```
Transient analysis
.tran 20m uic
.plot tran V(out)
.plot tran V(gate)
.plot tran V(ctrl)
```

Bode Frequency Response analysis

```
.bode Vperturb 20m 50 5K 80m
.bode Rt 20m 50 5K 80m
.option bodein=fb
.option bodeout=out
.option bodeampfreq=0
```



Syntax <AMP> and .option Bodeampfreq / BodeLoPow / BodeHiPow

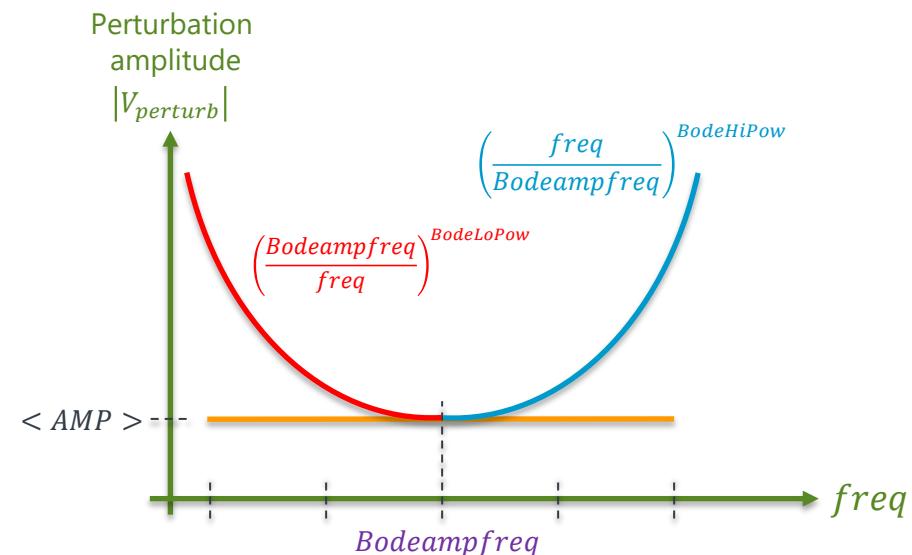
- Perturbing Source Signal Amplitude
 - In close-loop perturbing, it requires flexibility to change its amplitude across test frequency to boost signal in high attenuation region or prevent controller saturation

- .option Bodeampfreq

- If .option Bodeampfreq=0
 - $|V_{perturb}|$ for all frequency is unchanged = <AMP>
- If .option Bodeampfreq is not defined
 - Default $BodeAmpFreq = 10^{\frac{\log_{10}(Fstop) + \log_{10}(Fstart)}{2}}$
- If .option Bodeampfreq=<value>
 - $BodeAmpFreq = < f_{bodeampfreq} >$

- .option BodeLoPow and BodeHiPow (Default as 1)

- Assume $freq$ is between <Fstart> and <Fstop>
- If $freq < Bodeampfreq$: $|V_{perturb}| = < AMP > \left(\frac{Bodeampfreq}{freq} \right)^{BodeLoPow}$
- If $freq \geq Bodeampfreq$: $|V_{perturb}| = < AMP > \left(\frac{freq}{Bodeampfreq} \right)^{BodeHiPow}$



Syntax <AMP> and .option Bodeampfreq / BodeLoPow / BodeHiPow

Qspice : bode - bodehipow bodelopow formula.qsch

- BodeLoPow / BodeHiPow
 - Formula is implemented in this schematic to demonstrate amplitude profile by changing BodeLoPow and BodeHiPow
 - ** In default, $\text{BodeLoPow}=\text{BodeHiPow}=1$
 - .option Bodeampfreq=0 force to constant amplitude

.bode and .option parameters

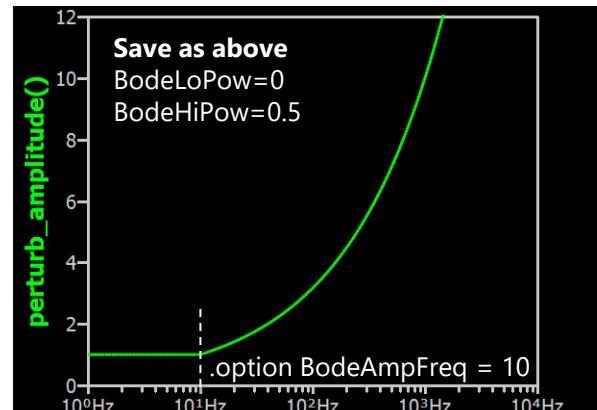
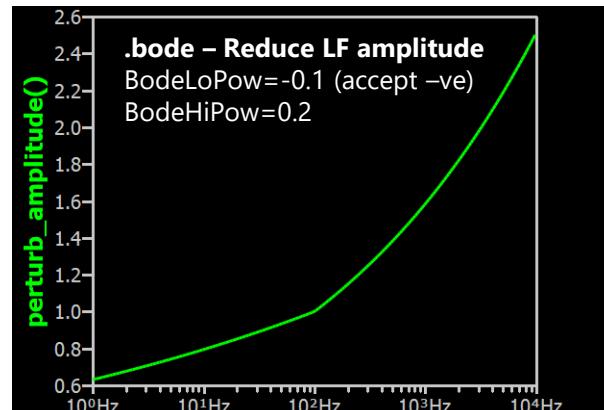
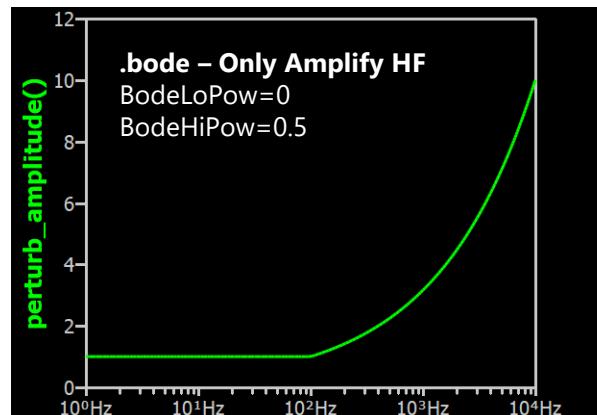
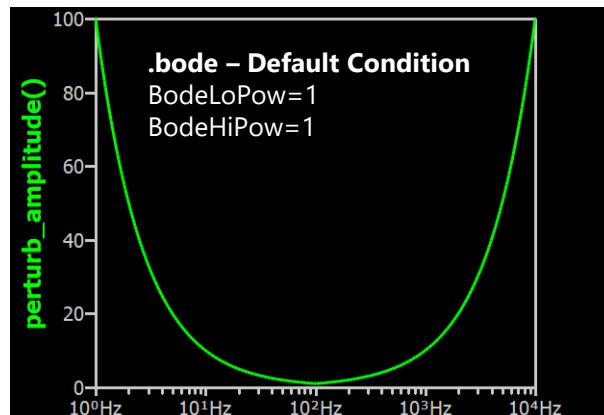
```
.param Amp = 1 ; [AMP] in .bode
.param Fstart = 1 ; [Fstart] in .bode
.param Fstop = 1e4 ; [Fstop] in .bode
.param BodeAmpFreq = pow(10,(log10(Fstop)+log10(Fstart))/2) ; default
.param BodeAmpFreq = 20 ; manual define BodeAmpFreq in .option
```



```
.param BodeLoPow = 1
.param BodeHiPow = 1
```

Calculate Amplitude vs Frequency Profile

```
.ac dec 100 Fstart Fstop
.func perturb_amplitude() AMP*if(Freq/BodeAmpFreq<1,
+pow(BodeAmpFreq/Freq, BodeLoPow),
+pow(Freq/BodeAmpFreq, BodeHiPow))
.plot perturb_amplitude()
```

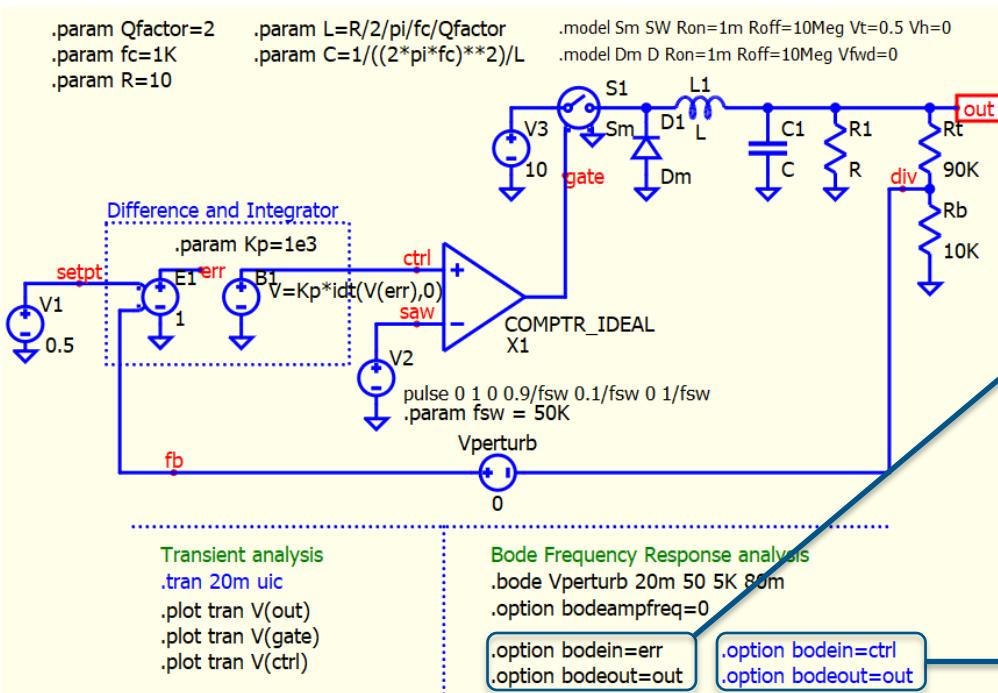


.option Bodein and Bodeout

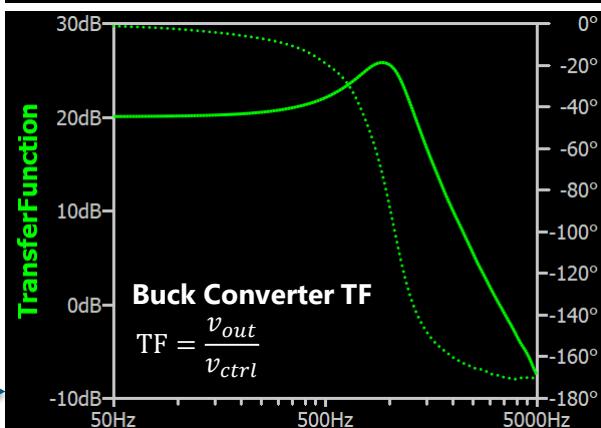
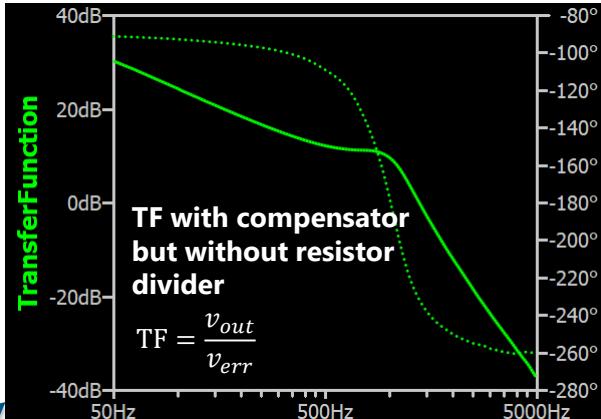
Qspice : bode - bodein bodeout.qsch

Bodein and Bodeout

- User can define voltage note name for bodein/bodeout params, result is store as TransferFunction



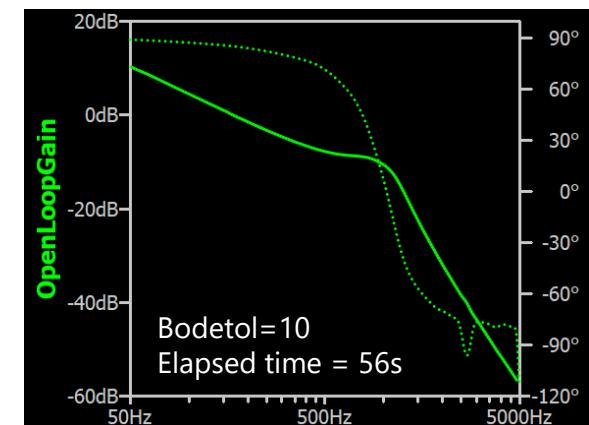
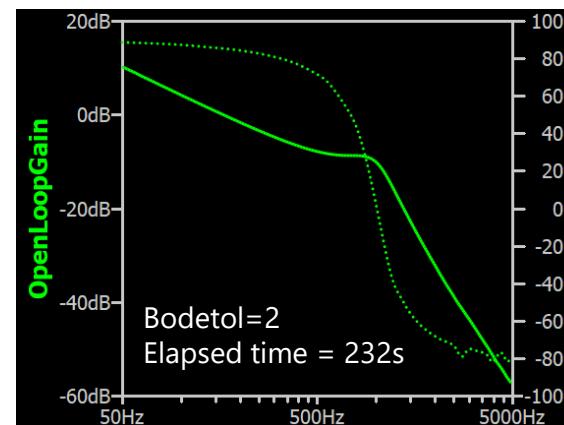
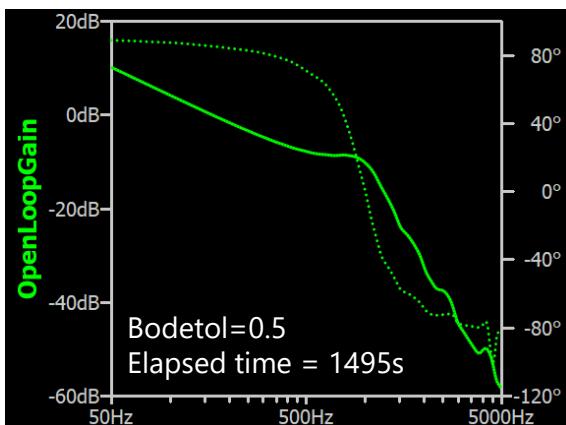
$$\text{TransferFunction} = \frac{\text{bodeout}}{\text{bodein}}$$



.option Bodetol

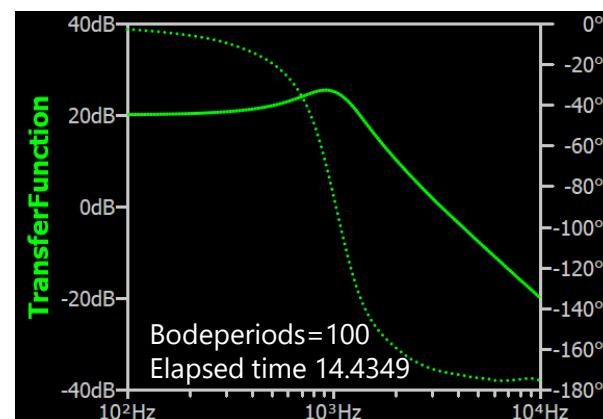
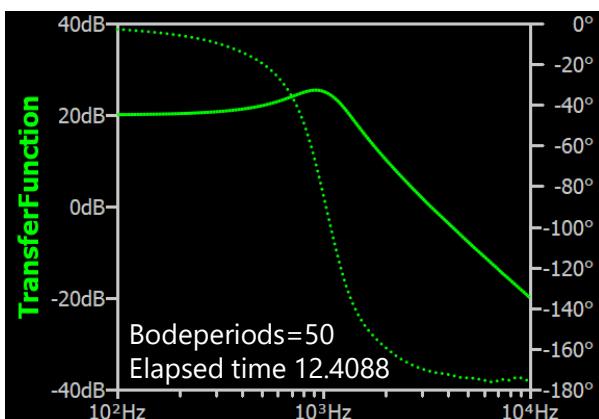
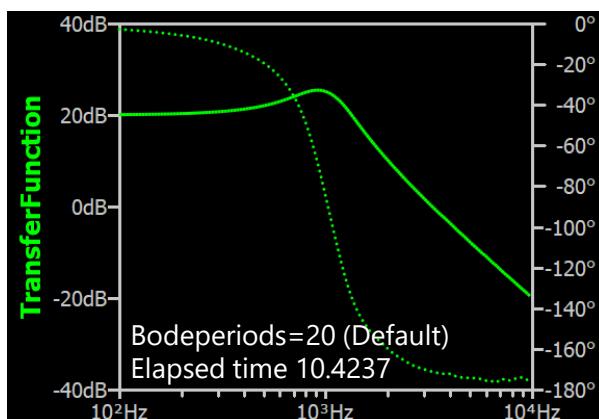
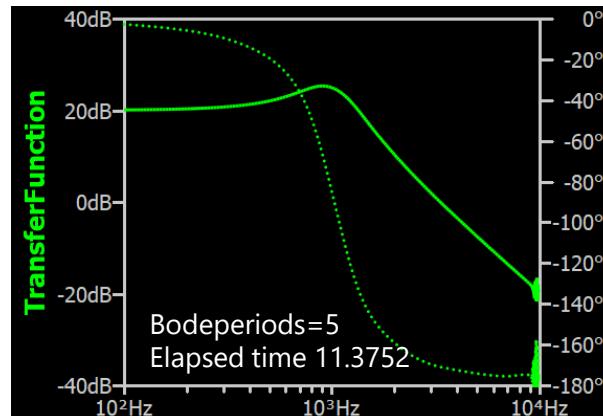
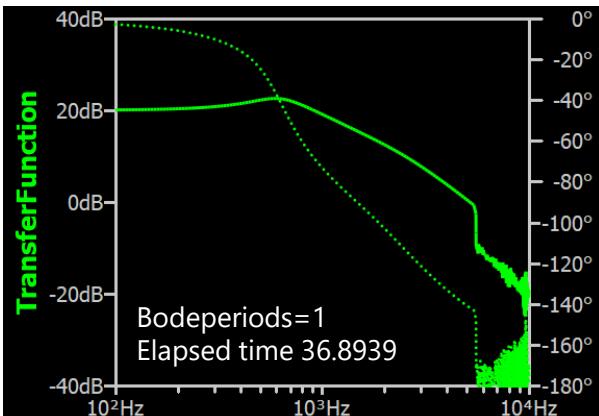
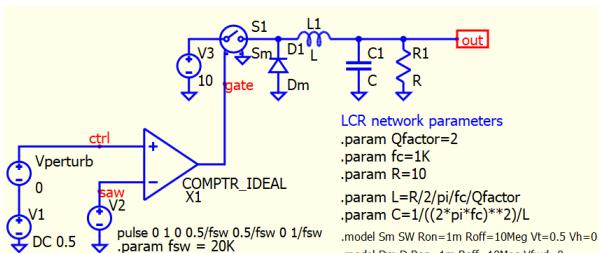
Qspice : bode - bodetol.qsch

- Bodetol : A frequency response analysis relative tolerance
 - Default Bodetol=10
 - Acceptable value from 0.1 to 15
 - Bodetol affects duration of time domain simulation during .bode
 - lower value = longer .tran duration = increase of simulation time
 - Reduce this value to to sharpen the gain profile for a high Q transfer function
 - Reduce Bodetol may improve simulation results, but this is not guarantee if decrease too much!



.option Bodeperiods

Qspice : bode - Buck - open loop - bodeperiods.qsch



** I cannot identify it exact function, but setting in default can give a reasonable result

**Explain .ac and .bode
relationship**

Basic of Frequency Response Analysis

Qspice : Bode - LCR - open loop.qsch

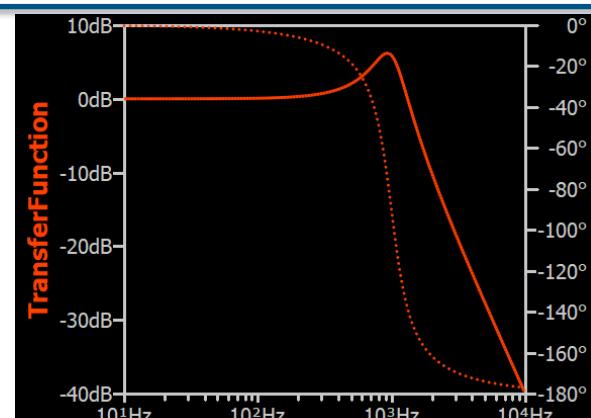
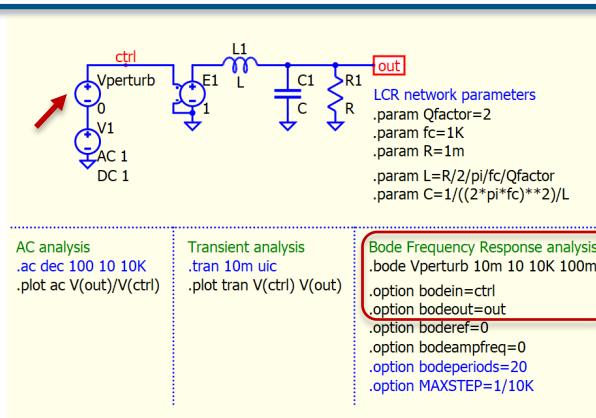
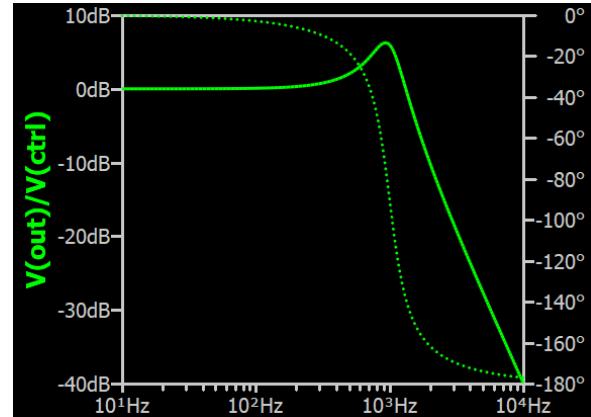
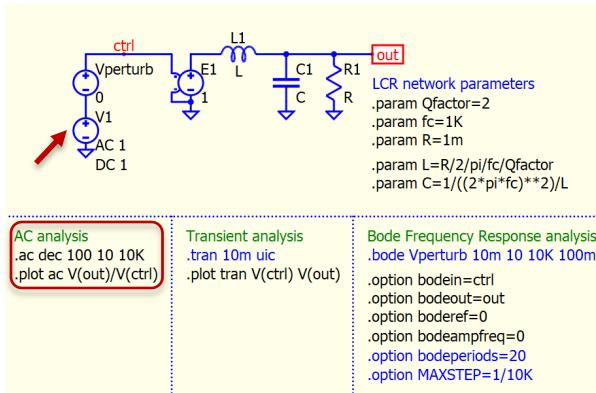
- Basic Theory

- Frequency response analysis is to insert a perturbing source into system, and measuring gain/phase between two voltage nodes
- .ac and .bode can achieve same result for linear circuit
- In .ac example, V1 has AC 1 as perturbation source, and

$$G(s) = \frac{v_{out}}{v_{ctrl}}$$

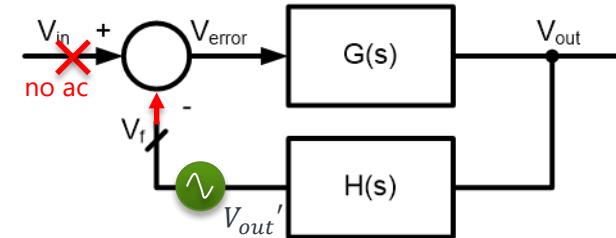
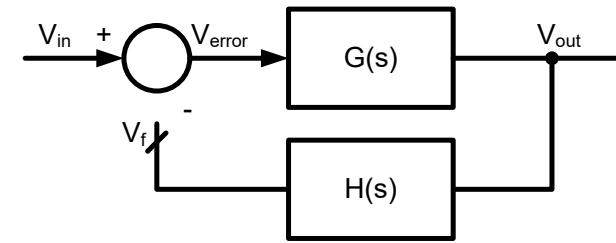
- In .bode example, Vperturb is inserted with a setting that voltage equals 100mV from 10Hz to 10kHz

$$G(s) = \frac{\text{bodeout}}{\text{bodein}} = \frac{v_{out}}{v_{ctrl}}$$



Open Loop Transfer Function in Close Loop System : Theory

- For close-loop system, perturbing source is added in feedback path to measure its open loop transfer function without breaking the close-loop operation
- Definition of Open Loop Transfer Function
 - It is defined as cutting the feedback path as
 - $GH(s) = G(s)H(s) = G_c(s)G_{plant}(s)H(s)$
- When V_f is break from the loop and AC test signal is from V_{in}
 - $GH(s) = \frac{\text{output of } H(s)}{\text{input of } G(s)} = \frac{\tilde{v}_f}{\tilde{v}_{in}} = \frac{\tilde{v}_f}{\tilde{v}_{error}}$
- If V_{in} is DC only and inject an AC to feedback path as test signal
 - $\tilde{v}_{error} = -\tilde{v}_f$
 - $GH(s) = \frac{\text{output of } H(s)}{\text{input of } G(s)} = \frac{\tilde{v}_{out'}}{\tilde{v}_{error}} = -\frac{\tilde{v}_{out'}}{\tilde{v}_f}$
 - If $H(s) = 1$, $V_{out} = V_{out'}$
 - $GH(s) = G_c(s)G_{plant}(s) = \frac{\tilde{v}_{out}}{\tilde{v}_{error}} = -\frac{\tilde{v}_{out}}{\tilde{v}_f}$

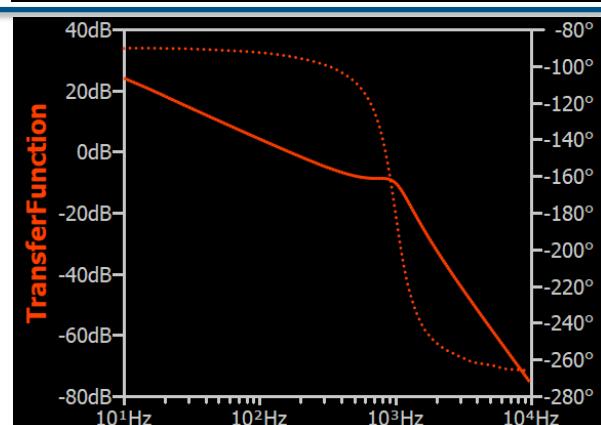
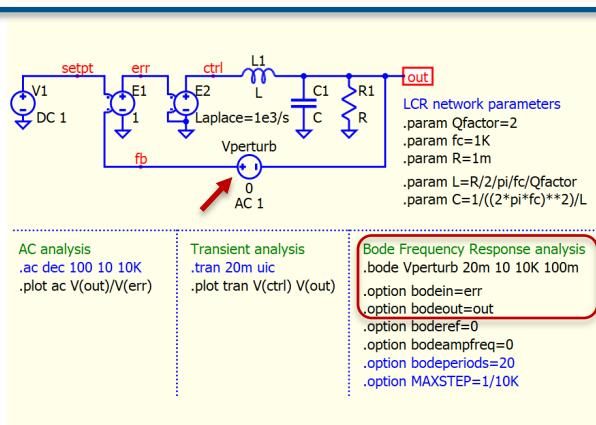
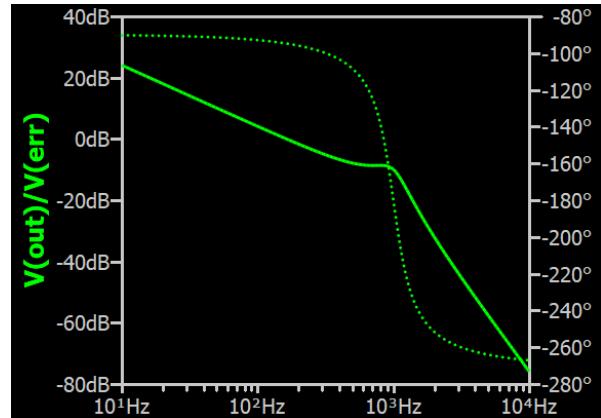
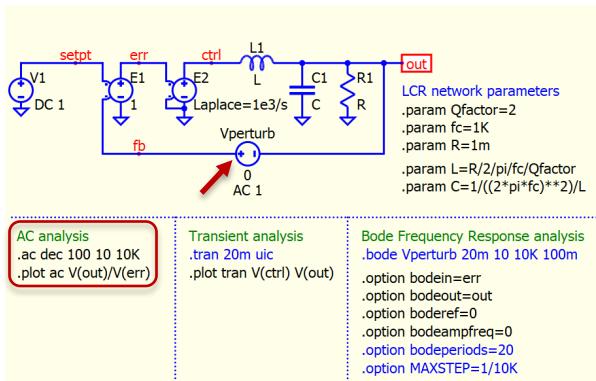


Open Loop Transfer Function in Close Loop System

Qspice : Bode - LCR - open loop.qsch

- Open Loop Transfer Function in Close Loop System

- Perturbing source is inserted into feedback path
- Open Loop Transfer Function
$$GH(s) = -\frac{v_{out}}{v_f} = \frac{v_{out}}{v_{err}}$$
- This is a linear system example, with E1 as difference and E2 as compensator (integrator), both .ac and .bode can be used in analyzing linear system



Appendix

Step-by-Step Example A Buck Converter

Part 1 : Close Loop Bode Plot Example

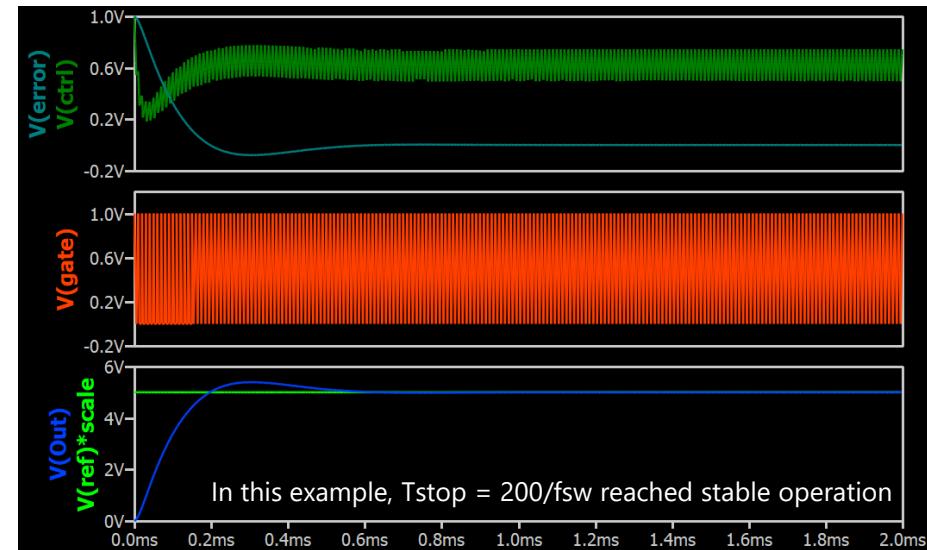
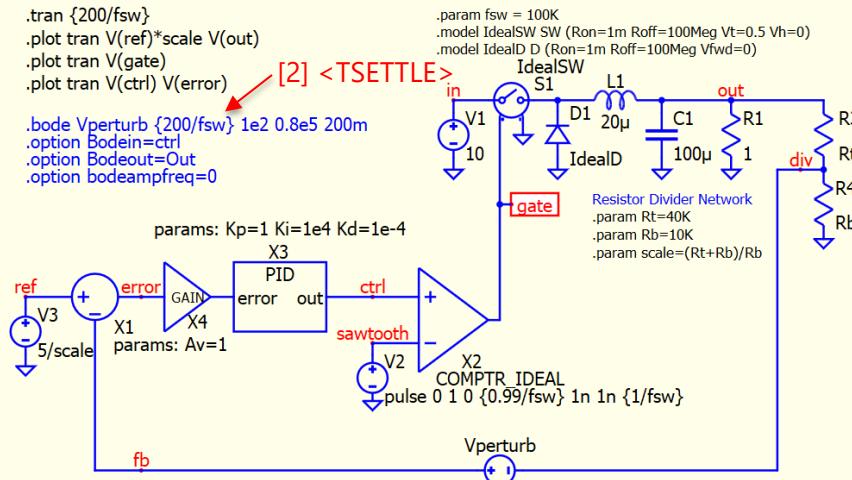
Qspice : Buck CloseLoop with Vperturb (.tran).qsch

- Determine <Tsettle>
 - [1] Run .tran analysis to determine how long the circuit can settle to steady state
 - .bode can only perform for a stable system
 - [2] Time required to reach stable operation is <TSETTLE> for .bode directive

Close Loop Feedback for Buck Converter with Bode Plot Analysis

```
.tran {200/fsw}
.plot tran V(ref)*scale V(out)
.plot tran V(gate)
.plot tran V(ctrl) V(error)
.bode Vperturb {200/fsw} 1e2 0.8e5 200m
```

[2] <TSETTLE>



Part 1 : Close Loop Bode Plot Example - <SOURCE> is voltage source

Qspice : Buck CloseLoop with Vperturb (.bode).qsch

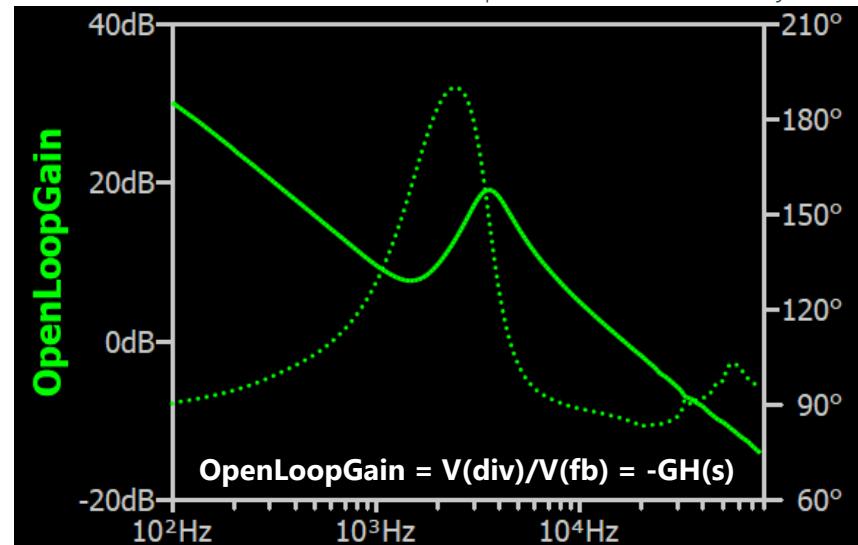
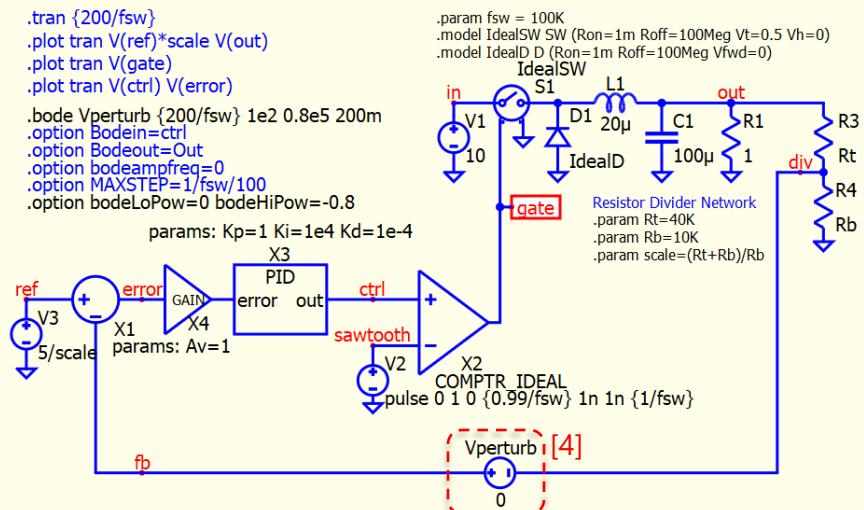
- .bode simulation with <SOURCE> is voltage source
 - [1] User determine <FSTART>, <FSTOP> and <AMP>, in this example, variable amplitude is used
 - [2] Perturbing source is added in series to feedback loop
 - If .option bodein and bodeout not specify
 - Bodeout is -ve terminal : transfer function numerator voltage node (e.g. div)
 - Bodein is +ve terminal : transfer function denominator voltage node (e.g. fb)
 - [3] Run simulation to get bode plot
 - If OpenLoopGain is not smooth, consider to adjust bodeLoPow and bodeHiPow for Amplitude <AMP> of perturbing source
 - If instability is observed at certain frequency, can use .option MAXSTEP to limit maximum time step in time domain analysis

Close Loop Feedback for Buck Converter with Bode Plot Analysis

```
.tran {200/fsw}
.plot tran V(ref)*scale V(out)
.plot tran V(gate)
.plot tran V(ctrl) V(error)

.bode Vperturb {200/fsw} 1e2 0.8e5 200m
.option Bodein=ctrl
.option Bodeout=Out
.option bodeampfreq=0
.option MAXSTEP=1/fsw/100
.option bodeLoPow=0 bodeHiPow=-0.8

params: Kp=1 Ki=1e4 Kd=1e-4
```



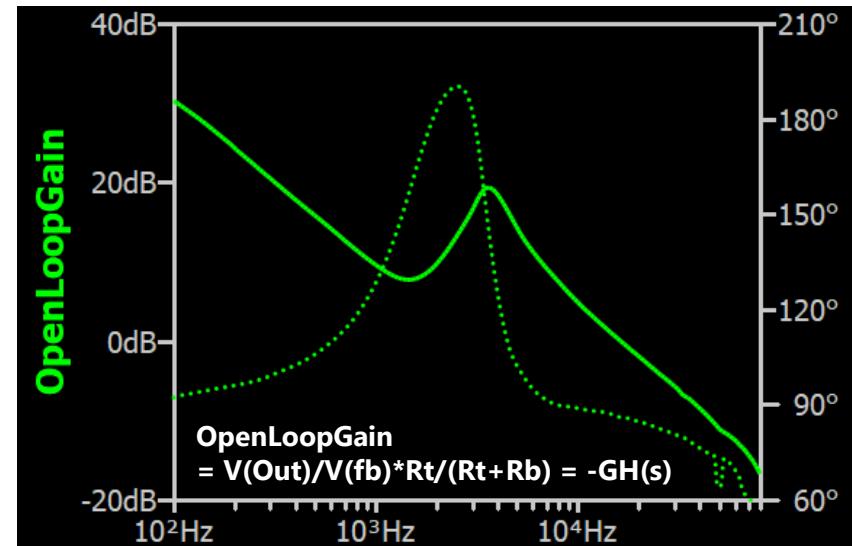
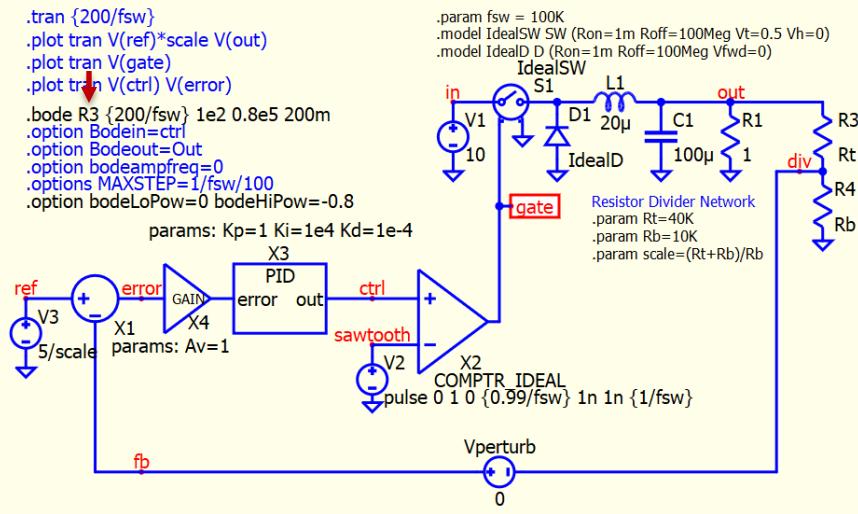
Part 1 : Close Loop Bode Plot Example - <SOURCE> is Top Resistor

Qspice : Buck CloseLoop with R3 (.bode).qsch

- .bode simulation with <SOURCE> is Top Resistor
 - [1] Alternatively, top resistor can be used as the perturbing source <SOURCE>
 - Resistor Pin 1 : transfer function numerator voltage node (e.g. out)
 - Resistor Pin 2 : transfer function denominator voltage node (e.g. div=fb)
 - [2] Run simulation to get bode plot

Close Loop Feedback for Buck Converter with Bode Plot Analysis

```
.tran {200/fsw}
.plot tran V(ref)*scale V(out)
.plot tran V(gate)
.plot tran V(ctrl) V(error)
.bode R3 {200/fsw} 1e2 0.8e5 200m
.option Bodein=ctrl
.option Bodeout=Out
.option bodeampfreq=0
.options MAXSTEP=1/fsw/100
.option bodeLoPow=0 bodeHiPow=-0.8
.params: Kp=1 Ki=1e4 Kd=1e-4
.ref V3 5/scale
.error X1
.error X4
.params: Av=1
.error out
.ctrl sawtooth
.error X2
.error COMPTR IDEAL
.pulse 0 1 0 {0.99/fsw} 1n 1n {1/fsw}
```

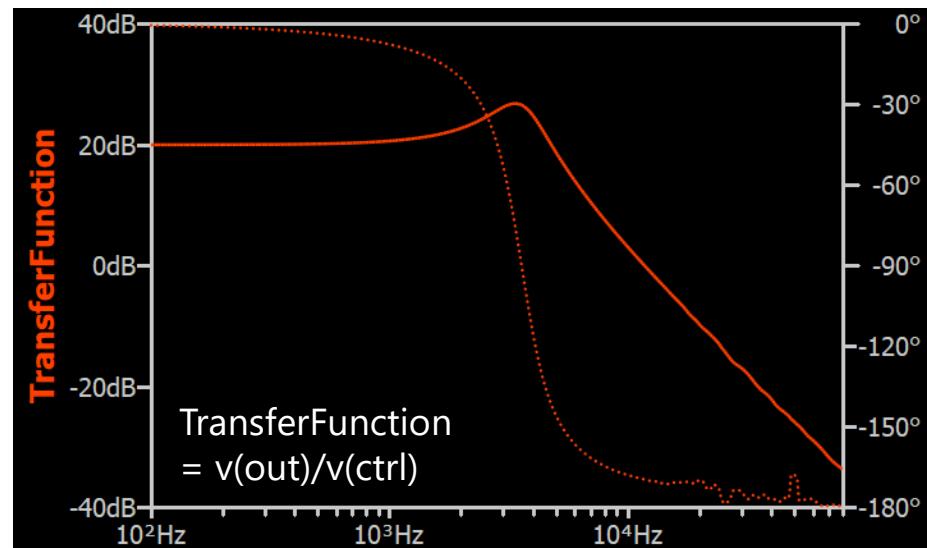
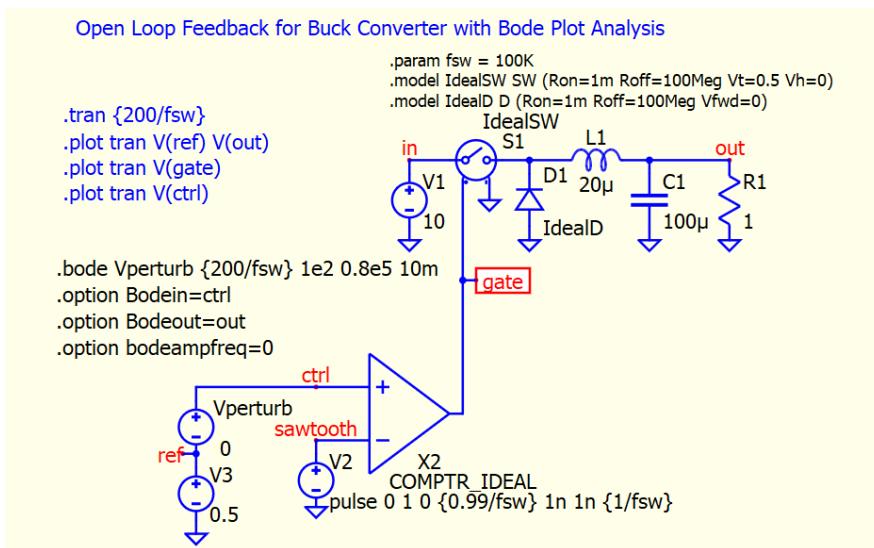


Part 2 : Open Loop Bode Plot Example

Qspice : Buck OpenLoop with Vperturb (.bode).qsch

- .bode for Open Loop

- As numerator and denominator voltage node can be defined by in .option bodein / bodeout
- [1] Arrange circuit into open loop operation, add perturbing source in series of reference/setpoint to input node (e.g. ctrl in this example)
- [2] use .option to set input node with **.option Bodein** and output node with **.option Bodeout**
- [3] Run simulation to get bode plot



Part 2 : Open Loop Bode Plot Example – C++ Comparator Block

Qspice : Buck ConverterBodePlot - OpenLoop with Cpp.qsch

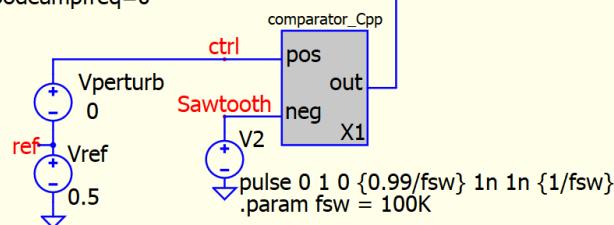
- .bode for Open Loop with a C++ Comparator Block
 - This is to demonstrate .bode can work with digital blockset

Buck Converter Bode with Open Loop

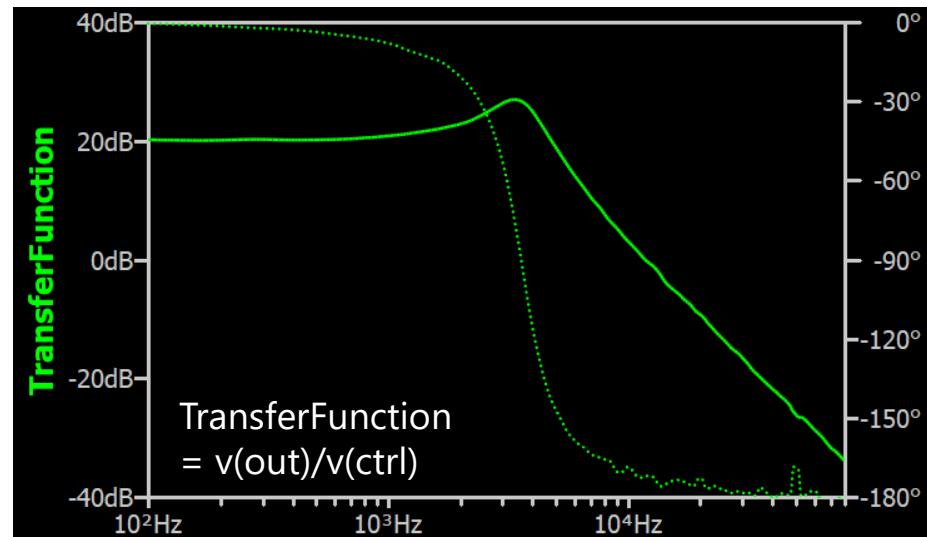
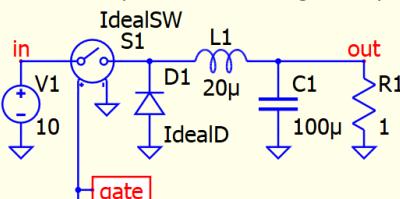
```
.tran {200/fsw}  
.plot V(out)  
.plot V(gate)
```

```
.options MAXSTEP={1/fsw/50}
```

```
.bode Vperturb {200/fsw} 1e2 0.8e5 20m  
.options bodein=ctrl  
.options bodeout=out  
.options bodeampfreq=0
```



```
.model IdealSW SW (Ron=1m Roff=100Meg Vt=0.5 Vh=0)  
.model IdealD D (Ron=1m Roff=100Meg Vfwd=0)
```



Appendix B

Qspice Demo :

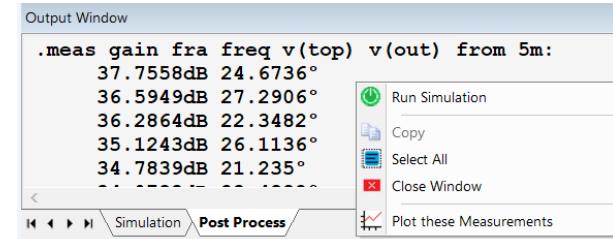
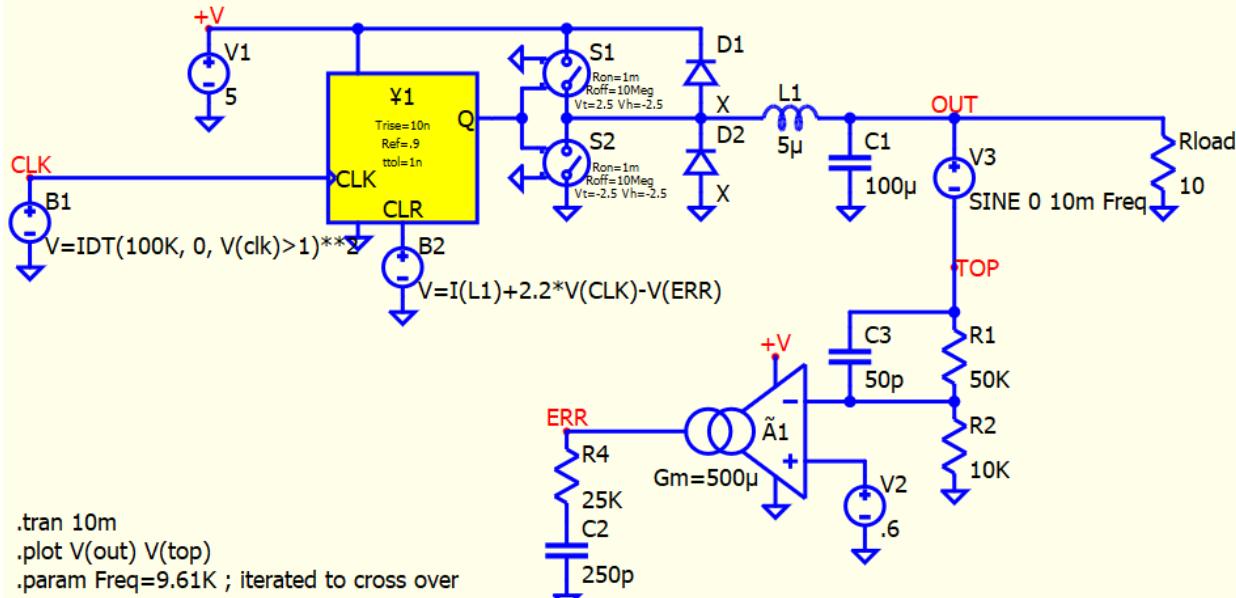
FRA_SMPS

Compare FRA and .bode

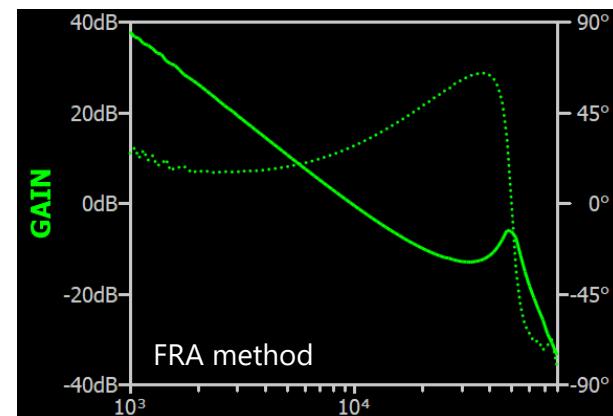
Use Qspice Demo Circuit FRA_SMPS.qsch to compare FRA and .bode

Qspice : FRA_SMPS (fra).qsch

Example of using the .meas FRA command. Probably the most accurate way of extracting the open loop voltage gain at a specific frequency.



[2] In Post Process
Right Click > Plot these Measurements
This will generate below Bode Plot

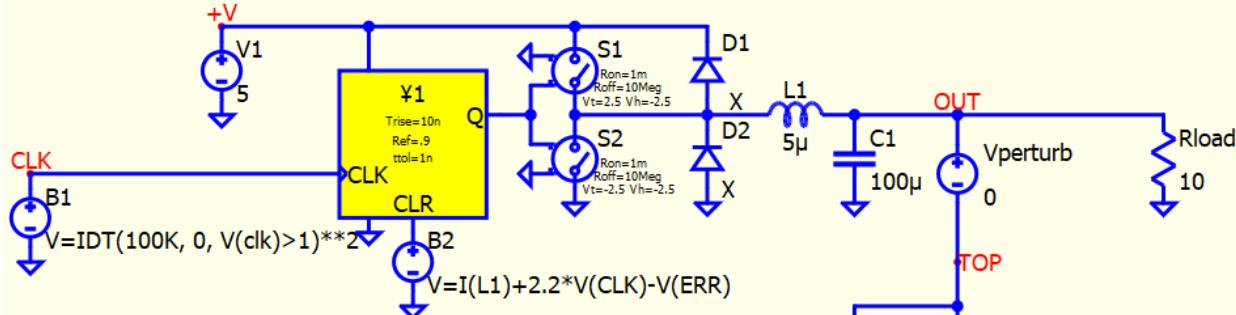


Total elapsed time : 43.0839 seconds

Use Qspice Demo Circuit FRA_SMPS.qsch to compare FRA and .bode

Qspice : FRA_SMPS (.bode).qsch

Example of using the .meas FRA command. Probably the most accurate way of extracting the open loop voltage gain at a specific frequency.



```
.bode Vperturb 5m 1K 80K 10m
.options bodein=top
.options bodeout=out
.options bodelopow=1 bodehipow=-0.3
.options bodeampfreq=0 ; enable for fixed amplitude
.option bodeltol=2 ; set bodeltol=2 for more precise result
```

Total elapsed time : 7.3703 seconds

- Bodelopow and bodehipow are used to fit a better perturbing amplitude profile
- Bodeltol set to lower value for more precise result

